

# Linear Systems, 2019 - Lecture 1

- Introduction
- Multivariable Time-varying Systems
- Transition Matrices
- Controllability and Observability
- Realization Theory
- Stability Theory
- Linear Feedback
- Multivariable input/output descriptions
- Some Bonus Material

# Lecture 1

- State equations
- Linearization
- Examples
- Transition matrices

Rugh, chapters 1-4

Main news:

- Linearization around trajectory
- Transition matrix  $\Phi(t, \tau)$

# Linear Time-Invariant (LTI) System

## State Representation

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t), & x(0) &= 0 \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$

## Convolution Representation

$$\begin{aligned}y(t) &= \int_0^t G(t - \tau)u(\tau)d\tau \\ G(t) &= Ce^{At}B + \delta(t)D \quad (\text{impulse response})\end{aligned}$$

## Transfer Function Representation

$$\begin{aligned}\mathbf{y}(s) &= \mathbf{G}(s)\mathbf{u}(s) \\ \mathbf{G}(s) &:= \int_{0-}^{\infty} e^{-st}G(t)dt = C(sI - A)^{-1}B + D\end{aligned}$$

# Time-varying Linear System

State Representation

$$\begin{aligned}\dot{x}(t) &= A(t)x(t) + B(t)u(t), & x(0) &= 0 \\ y(t) &= C(t)x(t) + D(t)u(t)\end{aligned}$$

Integral Representation

$$y(t) = \int_0^t G(t, \tau)u(\tau)d\tau + D(t)u(t)$$

Operator Representation

$$y = Lu$$

## Example: Two Tank System

Flow:  $q(t)$

Volumes:  $V_1, V_2$  (constant)

Concentrations:  $u(t), x_1(t), x_2(t)$

Dynamics:

$$\begin{cases} \frac{d}{dt}(V_1 x_1) &= qu - qx_1 \\ \frac{d}{dt}(V_2 x_2) &= qx_1 - qx_2 \end{cases}$$

$$\dot{x}(t) = \begin{bmatrix} -\frac{1}{V_1} & 0 \\ \frac{1}{V_2} & -\frac{1}{V_2} \end{bmatrix} q(t)x(t) + \begin{bmatrix} \frac{1}{V_1} \\ 0 \end{bmatrix} q(t)u(t)$$

## Example: Electric Circuit (RLC circuit)

See Fig 2.4

Capacitor Dynamics:

$$i(t) = \frac{d}{dt} (c(t)u_c(t))$$

Inductor Dynamics:

$$u_l(t) = \frac{d}{dt} (l(t)i(t))$$

State Representation:  $x = [u_c \ i]^T$

$$\dot{x}(t) = \begin{bmatrix} -\dot{c}/c & 1/c \\ -1/l & -(r + \dot{l})/l \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 1/l \end{bmatrix} u(t)$$

# Discrete Time LTI System

## State Representation

$$\begin{aligned}x(k+1) &= Ax(k) + Bu(k), & x(0) &= 0 \\y(k) &= Cx(k) + Du(k)\end{aligned}$$

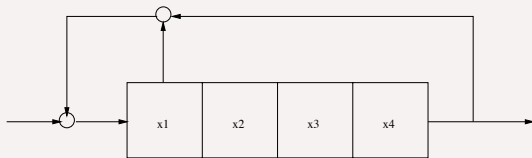
## Convolution Representation

$$y(k) = \sum_{l=0}^k G(k-l)u(l)$$
$$G(k) = \begin{cases} D & k = 0 \\ CA^{k-1}B & k \geq 1 \end{cases} \quad (\text{impulse response})$$

## Transfer Function Representation

$$\mathbf{y}(z) = \mathbf{G}(z)\mathbf{u}(z)$$
$$\mathbf{G}(z) := \sum_{k=0}^{\infty} G(k)z^{-k} = C(zI - A)^{-1}B + D$$

## Example: Shift Register



$$x = [x_1 \quad x_2 \quad x_3 \quad x_4]^T$$

$$x(k+1) = \begin{bmatrix} 1 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} x(k) + \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} u(k)$$

$$y(k) = [0 \quad 0 \quad 0 \quad 1] x(k)$$



# Linearization around a trajectory

Consider

$$\dot{x}(t) = f(x(t), u(t), t), \quad x(0) = x_0$$

with solution  $\tilde{x}(t)$  for  $u(t) = \tilde{u}(t)$  and  $x_0 = \tilde{x}_0$ .

Let  $x_\delta = x - \tilde{x}$ . Assuming differentiability of  $f$ ,

$$\begin{aligned} & f(\tilde{x} + x_\delta, \tilde{u} + u_\delta, t) - f(\tilde{x}, \tilde{u}, t) \\ &= \frac{\partial f}{\partial x}(\tilde{x}, \tilde{u}, t)x_\delta + \frac{\partial f}{\partial u}(\tilde{x}, \tilde{u}, t)u_\delta + o(|x_\delta|, |u_\delta|) \end{aligned}$$

Hence, with

$$A(t) = \frac{\partial f}{\partial x}(\tilde{x}, \tilde{u}, t), \quad B(t) = \frac{\partial f}{\partial u}(\tilde{x}, \tilde{u}, t)$$

the linearization around  $(\tilde{x}(t), \tilde{u}(t))$  is

$$\dot{x}_\delta(t) = A(t)x_\delta(t) + B(t)u_\delta(t), \quad x_\delta(0) = x_0 - \tilde{x}_0$$

## Example: Communications Satellite

Spherical coordinates:  $x = [r \dot{r} \theta \dot{\theta} \phi \dot{\phi}]^T$

Input:  $u = [u_r \ u_\theta \ u_\phi]^T$ , Output:  $y = [r \ \theta \ \phi]^T$

Dynamics:

$$\dot{x}(t) = f(x(t), u(t), t)$$

$$= \begin{bmatrix} \dot{r} \\ r\dot{\theta}^2 \cos^2 \phi + r\dot{\phi}^2 - k/r^2 + u_r/m \\ \dot{\theta} \\ -2\dot{r}\dot{\theta}/r + 2\dot{\theta}\dot{\phi} \sin \phi / \cos \phi + u_\theta \cos \phi / (mr) \\ \dot{\phi} \\ -\dot{\theta}^2 \cos \phi \sin \phi - 2\dot{r}\dot{\phi}/r + u_\phi / (mr) \end{bmatrix}$$

# Linearized Communications Satellite

Circular equatorial orbit:

$$\begin{aligned}\tilde{x} &= \begin{bmatrix} \tilde{r} & 0 & \tilde{\omega}t & \tilde{\omega} & 0 & 0 \end{bmatrix}^T \\ \tilde{u} &\equiv 0\end{aligned}$$

Linearization:  $\dot{x} = Ax + Bu$  with

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ \tilde{\omega}^2 - \frac{2k}{\tilde{\omega}^3} & 0 & 0 & 2\tilde{\omega}\tilde{r} & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & -2\tilde{\omega}/\tilde{r} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & -\tilde{\omega}^2 & 0 \end{bmatrix},$$
$$B = \begin{bmatrix} 0 & 0 & 0 \\ 1/m & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1/(m\tilde{r}) & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1/(m\tilde{r}) \end{bmatrix}$$

# Linearization in Matlab/Simulink

```
[X,U,Y,DX]=TRIM('SYS',X0,U0,Y0,IX,IU,IY)
```

fixes X, U and Y to X0(IX), U0(IU) and Y0(IY).

The variables IX, IU and IY are vectors of indices.

```
[A,B,C,D]=LINMOD('SYS',X,U)
```

allows the state vector, X, and input, U, to be specified. A linear model will then be obtained at this operating point.

# Linearization in Matlab/Simulink

The image displays a MATLAB 7.9.0 (R2009b) environment. The top window shows a Simulink model named 'linsys01'. The model consists of an input block 'In1', a summing junction with a minus sign, an integrator block labeled 'Integrator', a square root block labeled 'sqrt' and 'Math Function', and an output block 'Out1'. The signal flow is: In1 → Summing Junction (-) → Integrator → sqrt → Out1. The output of the sqrt block is also fed back into the summing junction.

The bottom window shows the MATLAB Command Window with the following commands and output:

```
>> [x,u,y] = trim('linsys01',1,3,1,[],1,1)
x =
    9.0000
u =
     3
Y =
    9.0000
>> [A,B,C,D] = linmod('linsys01',x,u)
A =
   -0.1667
B =
     1
C =
     1
D =
     0
fs >>
```

# LTV Systems - Fundamental Matrix

Can we find a counter-part to the exponential matrix

$$\Phi(t) = e^{tA}$$

for linear time-varying systems?

What properties of the LTI case carry over to LTV systems?

# Discrete Time Systems

Given a matrix sequence  $A(0), A(1), \dots$  the equation

$$x(k+1) = A(k)x(k), \quad x(k_0) = x_0$$

has the unique solution

$$x(k) = \Phi(k, k_0)x_0$$

defined by the *transition matrix*

$$\Phi(k, k_0) = \begin{cases} A(k-1) \cdots A(k_0), & k > k_0 \\ I, & k = k_0 \end{cases}$$

Proof by inspection.

What about continuous time?

# Continuous Time-varying Linear Systems

$$\dot{x}(t) = A(t)x(t), \quad x(t_0) = x_0$$

is equivalent to the integral equation

$$x(t) = x_0 + \int_{t_0}^t A(s)x(s)ds$$

Under weak conditions on  $A(t)$  one can show convergence of

$$x_{k+1}(t) := x_0 + \int_{t_0}^t A(s)x_k(s)ds$$

$A(t)$  locally integrable (for instance bounded) is sufficient for existence and uniqueness

From the integral equation it is easy to see that the solution  $x(t)$  depends linearly on  $x(t_0)$  (how?)



# Continuous Time Systems

For bounded  $A(t)$ , the equation

$$\dot{x}(t) = A(t)x(t), \quad x(t_0) = x_0$$

hence has a unique solution of the form

$$x(t) = \Phi(t, t_0)x_0$$

The *transition matrix* can be written as the infinite sum

$$\begin{aligned}\Phi(t, t_0) &= I + \int_{t_0}^t A(\sigma_1)d\sigma_1 \\ &+ \int_{t_0}^t A(\sigma_1) \int_{t_0}^{\sigma_1} A(\sigma_2)d\sigma_2d\sigma_1 \\ &+ \int_{t_0}^t A(\sigma_1) \int_{t_0}^{\sigma_1} A(\sigma_2) \int_{t_0}^{\sigma_2} A(\sigma_3)d\sigma_3d\sigma_2d\sigma_1 \\ &\dots\end{aligned}$$

## Example: Time-invariant System

For

$$\dot{x} = Ax(t), \quad x(t_0) = x_0$$

the transition matrix is

$$\begin{aligned}\Phi(t, t_0) &= I + \int_{t_0}^t A d\sigma_1 + \int_{t_0}^t A \int_{t_0}^{\sigma_1} A d\sigma_2 d\sigma_1 + \dots \\ &= I + A(t - t_0) + A^2 \frac{(t - t_0)^2}{2} + A^3 \frac{(t - t_0)^3}{6} + \dots \\ &= e^{A(t-t_0)}\end{aligned}$$

so the solution is

$$x(t) = e^{A(t-t_0)} x_0$$

## Calculation of $\exp(At)$ by Jordan Form

From Matrix Theory: Transformation  $P$  exist so  $A = PJP^{-1}$  where  $J$  is a block diagonal matrix, each block being of the form

$$\lambda I + N = \begin{bmatrix} \lambda & 1 & 0 & \dots \\ 0 & \lambda & 1 & \dots \\ & & \ddots & 1 \\ 0 & \dots & 0 & \lambda \end{bmatrix}$$

Therefore  $e^{At} = Pe^{Jt}P^{-1}$  where  $e^{Jt}$  is a block diagonal matrix, each block having form

$$e^{(\lambda I + N)t} = e^{\lambda t} e^{Nt} = e^{\lambda t} \sum_k \frac{t^k}{k!} N^k = \begin{bmatrix} e^{\lambda t} & te^{\lambda t} & \frac{t^2}{2!}e^{\lambda t} & \dots \\ 0 & e^{\lambda t} & te^{\lambda t} & \ddots \\ & & \ddots & \\ 0 & \dots & 0 & e^{\lambda t} \end{bmatrix}$$

## WARNING - Common Mistakes in LTV Systems

If  $A(t)$  is time-varying, then in general

$$\Phi(t, t_0) \neq \exp \left\{ \int_{t_0}^t A(\sigma) d\sigma \right\}$$

Also beware that in general

$$e^{(A+B)t} \neq e^{At} e^{Bt}$$

Exception: If  $AB = BA$  then  $e^{(A+B)t} = e^{At} e^{Bt}$  holds (exercise)

## Warning: Stability is NOT determined by eigenvalues

Stability for a time-varying system

$$\dot{x} = A(t)x$$

can NOT be determined by the eigenvalues of  $A(t)$

For stability, location of the eigenvalues

$$\lambda(A(t))$$

in the left half plane for all  $t$  is neither sufficient or necessary!

Try to figure out a counter-example yourself!

(There will be one in Lecture 2)