Input-Output Models

Real-Time Systems, Lecture 7

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[IFAC PB Ch 3 p 22-34]

- Shift operators; the pulse transfer operator
- Z-transform; the pulse transfer function
- Transformations between system representations
- System response, frequency response
- ZOH sampling of a transfer function

Linear System Models

		State-space model	Input-output models	
		y System	u System	<i>y</i>
			Differential/difference equation	Transfer operator/fcn
	ст	$\dot{x}(t) = Ax(t) + Bu(t)$ $y(t) = Cx(t)$	$\frac{\frac{d^n y}{dt^n} + a_1 \frac{d^{n-1} y}{dt^{n-1}} + \dots + a_n y}{= b_1 \frac{d^{n-1} u}{dt^{n-1}} + \dots + b_n u}$	$G(p) \ / \ G(s)$
$\begin{array}{c c} \mathbf{DT} & x(k+1) = \\ y(k) = \end{array}$		$x(k+1) = \Phi x(k) + \Gamma u(k)$ $y(k) = Cx(k)$	$y(k) + a_1 y(k-1) + \dots +$ $a_n y(k-n) = b_1 u(k-1)$ $+ \dots + b_n u(k-n)$	H(q) / H(z)

More I-O models: (im)pulse response, step response, frequency response

Operators on time series

The sampling period is chosen as the time unit $(f(k) \Leftrightarrow f(kh))$ Time series are doubly infinite sequences:

• $f(k): k = \ldots -1, 0, 1, \ldots$

Forward shift operator:

- denoted q
- qf(k) = f(k+1)
- $q^n f(k) = f(k+n)$

Backward shift operator:

- denoted q^{-1}
- $q^{-1}f(k) = f(k-1)$
- $q^{-n}f(k) = f(k-n)$

Rewrite the state-space model using the forward shift operator:

$$x(k+1) = qx(k) = \Phi x(k) + \Gamma u(k)$$
$$y(k) = Cx(k) + Du(k)$$

Eliminate x(k):

$$\begin{aligned} x(k) &= (qI - \Phi)^{-1} \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) = C(qI - \Phi)^{-1} \Gamma u(k) + Du(k) \\ &= \left[C(qI - \Phi)^{-1} \Gamma + D \right] u(k) = H(q)u(k) \end{aligned}$$

H(q) is the *pulse transfer operator* of the system Describes how the input and output are related. The pulse transfer function is a rational function

$$H(q) = \frac{B(q)}{A(q)}$$

deg A = n = the number of states deg $B = n_b \le n$ (otherwise the system would be acausal)

A(q) is the characteristic polynomial of Φ , i.e.

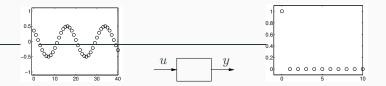
 $A(q) = \det(qI - \Phi)$

The *poles* of the system are given by A(q) = 0The *zeros* of the system are given by B(q) = 0 Poles:

• A pole in a is associated with the time function $f(k)=a^k\,$

Zeros:

- A zero in a implies that the transmission of the input $u(k)=a^k$ is blocked by the system
- Related to how inputs and outputs are coupled to the states



Recall the double integrator from the previous lecture:

$$\frac{dx}{dt} = \begin{bmatrix} 0 & 1\\ 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0\\ 1 \end{bmatrix} u$$
$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} x$$

Sample with h = 1:

$$\Phi = e^{Ah} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$
$$\Gamma = \int_0^h e^{As} B \, ds = \begin{bmatrix} 0.5 \\ 1 \end{bmatrix}$$

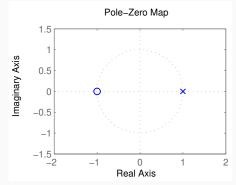
Disk Drive Example

Pulse transfer operator:

$$H(q) = C(qI - \Phi)^{-1}\Gamma + D$$

= $\begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} q - 1 & -1 \\ 0 & q - 1 \end{bmatrix}^{-1} \begin{bmatrix} 0.5 \\ 1 \end{bmatrix} = \frac{0.5(q+1)}{(q-1)^2}$

Two poles in 1, one zero in -1.



y(k) = H(q)u(k)A(q)y(k) = B(q)u(k)

$$(q^n + a_1q^{n-1} + \dots + a_n)y(k) = (b_0q^{n_b} + \dots + b_{n_b})u(k)$$

which means

$$y(k+n) + a_1 y(k+n-1) + \dots + a_n y(k)$$

= $b_0 u(k+n_b) + \dots + b_{n_b} u(k)$

$$y(k+n) + a_1y(k+n-1) + \dots + a_ny(k)$$

= $b_0u(k+n_b) + \dots + b_{n_b}u(k)$

can be written as

$$y(k) + a_1 y(k-1) + \dots + a_n y(k-n)$$

= $b_0 u(k-d) + \dots + b_{n_b} u(k-d-n_b)$

where $d = n - n_b$ is the *pole excess* of the system.

The reciprocal polynomial

$$A^*(q) = 1 + a_1q + \dots + a_nq^n = q^n A(q^{-1})$$

is obtained from the polynomial \boldsymbol{A} by reversing the order of the coefficients.

Now the system can instead be written as

$$A^*(q^{-1})y(k) = B^*(q^{-1})u(k-d)$$

Difference Equation Example

Using forward shift

$$y(k+2) + 2y(k+1) + 3y(k) = 2u(k+1) + u(k)$$

can be written

$$(q^2 + 2q + 3)y(k) = (2q + 1)u(k)$$

Hence,

$$A(q) = q^2 + 2q + 3$$
$$B(q) = 2q + 1$$

Using backward shift, the same equation can be written (d = 1)

$$(1+2q^{-1}+3q^{-2})y(k) = (2+q^{-1})u(k-1)$$

Hence,

$$A^*(q^{-1}) = 1 + 2q^{-1} + 3q^{-2}$$
$$B^*(q^{-1}) = 2 + q^{-1}$$

The discrete-time counterpart to the Laplace transform Defined on semi-infinite time series f(k) : k = 0, 1, ...

$$\mathcal{Z}{f(k)} = F(z) = \sum_{k=0}^{\infty} f(k)z^{-k}$$

z is a complex variable

Let
$$y(k)=1$$
 for $k\geq 0.$ Then
$$Y(z)=1+z^{-1}+z^{-2}+\cdots=\frac{z}{z-1}, \qquad |z|>1$$

Application of the following result for power series

$$\sum_{k=0}^{\infty} x^k = \frac{1}{1-x} \text{ for } |x| < 1$$

Z-transform Table

Table 2 (p 26) in IFAC PB (ignore the middle column!)

f	$\mathcal{L}f$	Zf
$\delta(k)$ (pulse)	_	1
1 $k \ge 0$ (step)	$\frac{1}{s}$	$\frac{z}{z-1}$
kh	$\frac{1}{s^2}$	$\frac{hz}{(z-1)^2}$
$\frac{1}{2} (kh)^2$	$\frac{1}{s^3}$	$\frac{h^2 z(z+1)}{2(z-1)^3}$
$e^{-kh/T}$	$\frac{T}{1+sT}$	$\frac{z}{z - e^{-h/T}}$
$1 - e^{-kh/T}$	$\frac{1}{s(1+sT)}$	$\frac{z(1-e^{-h/T})}{(z-1)(z-e^{-h/T})}$
$\sin \omega kh$	$\frac{\omega}{s^2 + \omega^2}$	$\frac{z\sin\omega h}{z^2 - 2z\cos\omega h + 1}$

$$\mathcal{Z}(\alpha f + \beta g) = \alpha F(z) + \beta G(z)$$
$$\mathcal{Z}(q^{-n}f) = z^{-n}F(z)$$
$$\mathcal{Z}(qf) = z(F(z) - f(0))$$
$$\mathcal{Z}(f * g) = \mathcal{Z}\left\{\sum_{j=0}^{k} f(j)g(k-j)\right\} = F(z)G(z)$$

$$\begin{cases} x(k+1) = \Phi x(k) + \Gamma u(k) \\ y(k) = Cx(k) + Du(k) \end{cases}$$

$$\begin{cases} z(X(z) - x(0)) = \Phi X(z) + \Gamma U(z) \\ Y(z) = CX(z) + DU(z) \end{cases}$$

$$Y(z) = C(zI - \Phi)^{-1}z x(0) + [C(zI - \Phi)^{-1}\Gamma + D]U(z)$$

The rational function $H(z) = C(zI - \Phi)^{-1}\Gamma + D$ is called the *pulse* transfer function from u to y.

It is the Z-transform of the pulse response h(k)

The pulse transfer operator ${\cal H}(q)$ and the pulse transfer function ${\cal H}(z)$ are the same rational functions

They have the same poles and zeros

- H(q) is used in the time domain (q =shift operator)
- H(z) is used in the Z-domain (z = complex variable)

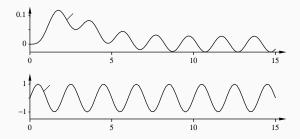
If the order of H(q) or H(z) is less than the order of the original state-space system, i.e., a pole-zero cancellation has taken place, then the system is either not reachable or not observable

- 1. Find the pulse transfer function $H(z)=C(zI-\Phi)^{-1}\Gamma+D$
- 2. Compute the Z-transform of the input: $U(z) = \mathcal{Z}\{u(k)\}$
- 3. Compute the Z-transform of the output:

$$Y(z) = C(zI - \Phi)^{-1}z x(0) + H(z)U(z)$$

4. Apply the inverse Z-transform (table) to find the output: $y(k) = \mathcal{Z}^{-1}\{Y(z)\}$

Frequency Response – Continuous Time

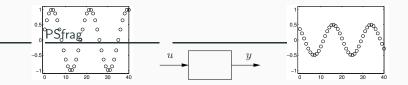


Given a stable system G(s), the input $u(t)=\sin\omega t$ will, after a transient, give the output

$$y(t) = |G(i\omega)| \sin\left(\omega t + \arg G(i\omega)\right)$$

- The amplitude and phase shift for different frequencies are given by the value of G(s) along the imaginary axes, i.e. $G(i\omega)$
- Plotted in Bode and Nyquist diagrams

Frequency Response – Discrete Time



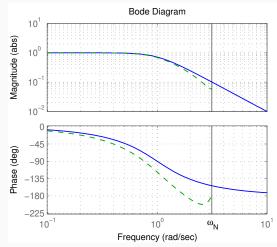
Given a stable system H(z), the input $u(k) = \sin(\omega k)$ will, after a transient, give the output

$$y(k) = |H(e^{i\omega})| \sin\left(\omega k + \arg H(e^{i\omega})\right)$$

- G(s) and the imaginary axis are replaced by H(z) and the unit circle.
- Only describes what happens at the sampling instants
- The inter-sample behavior is not studied in this course

Bode Diagram

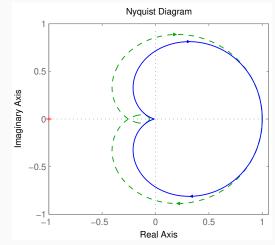
Bode diagram for $G(s) = 1/(s^2 + 1.4s + 1)$ (solid) and ZOH-sampled counterpart H(z) (dashed, plotted for $\omega h \in [0, \pi]$)



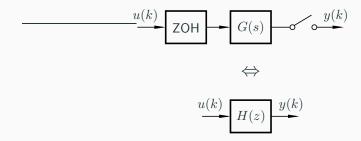
The hold circuit can be approximated by a delay of $\hbar/2$

Nyquist Diagram

Nyquist diagram for $G(s) = 1/(s^2 + 1.4s + 1)$ (solid) and ZOH-sampled counterpart H(z) (dashed, plotted for $\omega h \in [0, \pi]$)



ZOH Sampling of a Transfer Function



How to calculate H(z) given G(s)?

Three approaches:

- 1. Make a state-space realization of G(s). Sample using ZOH to obtain Φ and Γ . Then $H(z) = C(zI \Phi)^{-1}\Gamma + D$.
 - Works also for systems with time delays, $G(s)e^{-s\tau}$
- 2. Use the formula

$$H(z) = \frac{z-1}{z} \frac{1}{2\pi i} \int_{\gamma-i\infty}^{\gamma+i\infty} \frac{e^{sh}}{z-e^{sh}} \frac{G(s)}{s} ds$$
$$= \sum_{s=s_i} \frac{1}{z-e^{sh}} \operatorname{Res}\left\{\frac{e^{sh}-1}{s} G(s)\right\}$$

- s_i are the poles of G(s) and Res denotes the residue.
- outside the scope of the course

Calculation of H(z) Given G(s)

3. Use Table 3 (p 27) in IFAC PB

G(s)	$H(z) = \frac{b_1 z^{n-1} + b_2 z^{n-2} + \dots + a_n}{z^n + a_1 z^{n-1} + \dots + a_n}$	
$\frac{1}{s}$	$\frac{h}{z-1}$	
$\frac{1}{s^2}$	$\frac{h^2(z+1)}{2(z-1)^2}$	
e^{-sh}	z^{-1}	
	$\frac{1 - \exp(-ah)}{z - \exp(-ah)}$	
$\frac{a}{s(s+a)}$	a	$= \frac{1}{a} \left(1 - e^{-ah} - ahe^{-ah} \right)$ $= e^{-ah}$

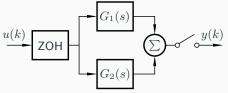
Example: For $G(s) = e^{-\tau s}/s^2$, the previous lecture gave

$$x(kh+h) = \Phi x(kh) + \Gamma_1 u(kh-h) + \Gamma_0 u(kh)$$
$$\Phi = \begin{pmatrix} 1 & h \\ 0 & 1 \end{pmatrix} \qquad \Gamma_1 = \begin{pmatrix} \tau \left(h - \frac{\tau}{2}\right) \\ \tau \end{pmatrix} \qquad \Gamma_0 = \begin{pmatrix} \frac{(h-\tau)^2}{2} \\ h-\tau \end{pmatrix}$$

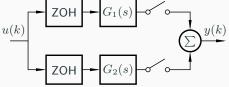
With h = 1 and $\tau = 0.5$, this gives

$$H(z) = C(zI - \Phi)^{-1}(\Gamma_0 + \Gamma_1 z^{-1}) = \frac{0.125(z^2 + 6z + 1)}{z(z^2 - 2z + 1)}$$

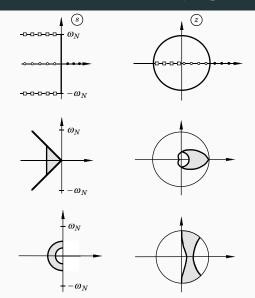
Order: 3 Poles: 0, 1, and 1 Zeros: $-3 \pm \sqrt{8}$ ZOH sampling is a linear operation, so a transfer function G(s) may be split into smaller parts $G_1(s) + G_2(s) + \ldots$ that are sampled separately





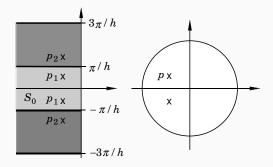


This does not hold for series decomposition, i.e., $\mathbb{ZOH}(G_1(s)G_2(s)) \neq \mathbb{ZOH}(G_1(s))\mathbb{ZOH}(G_2(s))$ Transformation of Poles via ZOH Sampling: $z_i = e^{s_i h}$



Note: The stability properties are preserved by ZOH sampling!

Several points in the s-plane are mapped into the same point in the z-plane. The map is not bijective



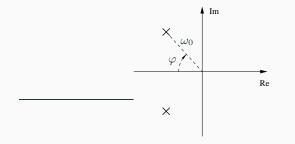
- More complicated than for poles
- Extra zeros may appear in the sampled system
- There can be zeros outside the unit circle (non-minimum phase) even if the continuous system has all the zeros in the left half plane
- For short sampling periods

 $z_i \approx e^{s_i h}$

ZOH Sampling of a Second Order System

Second order continuous-time system with complex poles:

$$G(s) = \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}, \qquad \zeta < 1$$



- Larger $\omega_0 \Rightarrow$ faster system response
- Smaller $\varphi \Rightarrow$ larger damping. Relative damping $\zeta = \cos \varphi$.
 - Common control design choice: $\zeta = \cos 45^\circ \approx 0.7$

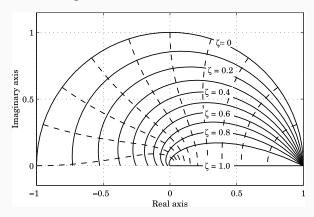
Sampled Second Order System

The poles of the sampled system are given by

$$z^2 + a_1 z + a_2 = 0$$

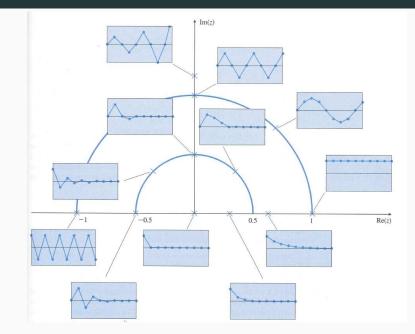
where

$$a_1 = -2e^{-\zeta\omega_0 h} \cos\left(\sqrt{1-\zeta^2}\,\omega_0 h\right)$$
$$a_2 = e^{-2\zeta\omega_0 h}$$



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Sampled Second Order System



Examples in Matlab

```
>> % From state space system to pulse transfer function
>> A = [0 \ 1; \ 0 \ 0];
>> B = [0; 1];
>> C = [1 \ 0]:
>> D = 0:
>> contsys = ss(A,B,C,D);
>> h = 1:
>> discsys = c2d(contsys,h);
>> tf(discsys) % pulse transfer function
>> zpk(discsys) % factored pulse transfer function
>> % Bode and Nyquist diagrams
>> s = tf('s'); G = 1/(s^2+1.4*s+1);
>> H = c2d(G,1);
>> bode(G.H)
>> nyquist(G,H)
>> % Sampling of a second-order transfer function
>> G = 1/(s^2+s+1);
>> h = 0.1:
>> H = c2d(G,h)
>> pzmap(H)
```